

Force-chain evolution in a two-dimensional granular packing compacted by vertical tappingsNaoki Iikawa,¹ M. M. Bandi,² and Hiroaki Katsuragi¹¹*Department of Earth and Environmental Sciences, Nagoya University, Furocho, Chikusa, Nagoya, Aichi 464-8601, Japan*²*Collective Interactions Unit, OIST Graduate University, Onna, Okinawa 904-0495, Japan*

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We experimentally study the statistics of force-chain evolution in a vertically-tapped two-dimensional granular packing by using photoelastic disks. In this experiment, the tapped granular packing is gradually compacted. During the compaction, the isotropy of grain configurations is quantified by measuring the deviator anisotropy derived from fabric tensor, and then the evolution of force-chain structure is quantified by measuring the interparticle forces and force-chain orientational order parameter. As packing fraction increases, the interparticle force increases and finally saturates to an asymptotic value. Moreover, the grain configurations and force-chain structures become isotropically random as the tapping-induced compaction proceeds. In contrast, the total length of force chains remains unchanged. From the correlations of those parameters, we find two relations: (i) a positive correlation between the isotropy of grain configurations and the disordering of force-chain orientations, and (ii) a negative correlation between the increasing of interparticle forces and the disordering of force-chain orientations. These relations are universally held regardless of the mode of particle motions with or without convection.

DOI: [10.1103/PhysRevE.97.032901](https://doi.org/10.1103/PhysRevE.97.032901)**I. INTRODUCTION**

Granular materials consist of discrete solid particles such as food grains or sand and show fluidlike and/or solidlike complex behavior due to the particle's discreteness and dissipative nature [1]. The packing fraction of granular materials ϕ is a relevant parameter for characterizing its structure and mechanical properties. In particular, granular states vary from fluidlike to solidlike around a packing fraction ϕ_{RCP} [2,3], called the random close packed state; $\phi_{RCP} = 0.84$ in a two-dimensional (2D) frictionless granular packing. According to previous studies [4,5], interparticle forces diverge near ϕ_{RCP} when a granular material is isotropically compressed. Other studies have indicated that the granular state depends not only on the packing fraction but also on the internal force conditions [6–8]. In granular materials, dissipative force transmits through the medium via contacting particles. This force transmission constructs the inhomogeneous stress distribution in a granular packing, called a “force chain” [9,10]. When a granular material is deformed under anisotropic loading such as shearing, a certain direction dominates the structure of the force chain. Then the force-chain structure becomes very anisotropic. In this case, interparticle forces diverge below ϕ_{RCP} . Thus, granular states deeply relate to the force-chain structure and its directional ordering. To reveal the relation between the granular state and force-chain structure in detail, recent studies have investigated the force-chain properties by varying the type of loadings and boundary conditions [11,12].

Here we focus on a different experimental setup: the force-chain structure in a granular packing subject to vertical tappings, which is different from isotropic compaction and shear deformation. In this study, we simply add a series of taps (one period of sinusoidal waveform) to the granular packing. In general, the tapped granular packing is gradually compacted [13]. Several studies have revealed that the compaction slowly proceeds up to the maximum packing fraction depending on

the tapping property [14,15]. This type of granular compaction occurs when the maximum tapping acceleration exceeds the magnitude of gravitational acceleration. In this condition, each particle can experience free fall, i.e., they are released from the gravitational constraint. Then, particles could form collective motions, such as granular convection, due to the existence of a free surface [16]. In the granular convective state, force chains are repeatedly reconstructed by the series of tappings. Although various external-loading dependences of the force-chain structure have been investigated [17], little is known about the relation between force-chain evolution and grain rearrangements caused by convective motion in vertically tapped granular packing.

Therefore, the main focus of this study is the evolution of force-chain structure in the granular compaction induced by tapping with and without convection. We perform experiments with 2D granular packing using photoelastic disks subject to vertical tapping. In a previous study, we developed a method to measure the interparticle force per disk F_d and force-chain segment length l by using bright- and dark-field images of photoelastic disks [18]. The force-chain orientational order parameter σ has also been introduced to quantify force-chain structure [19]. Using these quantities, the detailed structural properties of granular force chains in compaction and/or convection are characterized in this study.

II. METHOD**A. Experiment**

The experimental system consists of a 2D experimental chamber constructed with acrylic plates [Fig. 1(a)]. The chamber dimensions are $0.30 \times 0.30 \times 0.011$ m in height, width, and thickness, respectively. The chamber is attached to an electromagnetic shaker (EMIC Corp., model 513-B/A) which is connected to a multifunction generator (nf Corp., model

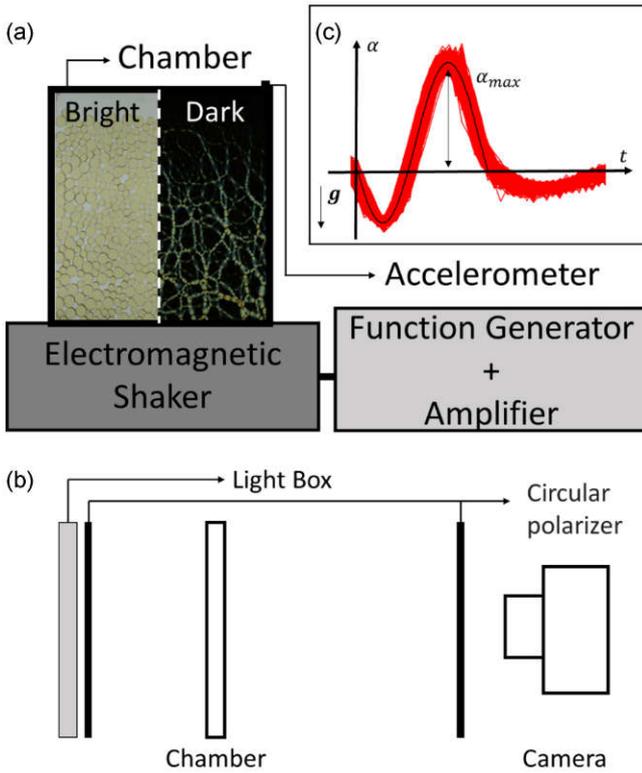


FIG. 1. (a) Schematic of the experimental setup. A chamber is filled with photoelastic disks. The chamber with an accelerometer is vertically mounted on an electromagnetic shaker connected to an amplifier and a multifunction generator. (b) Schematic of the optical system. Bright- and dark-field images are acquired by changing the optical setup (without or with a second polarizer). (c) Actual acceleration signals ($\Gamma = 5.0$ and $f = 50$ Hz) measured by the accelerometer. 1000 data sets are superimposed in the plot. The positive direction of the acceleration α is opposite to the direction of gravitational acceleration.

WF1974) through an amplifier (EMIC Corp., model 374A/G). An accelerometer (EMIC Corp., model 710-C) is mounted on a chamber to monitor its instantaneous acceleration induced by tapping. To avoid crystallization [19], we fill the chamber with a bidisperse set of 200 large (diameter 0.015 m) and 400 small (diameter 0.010 m) photoelastic disks of 0.010 m thickness (Vishay Micro Measurements, PSM-4). A circular polariscope setup is used for the optical system [Fig. 1(b)]. The chamber is vertically placed between a circular polarized light-emitting diode (LED) light source and a complementary metal oxide semiconductor (CMOS) camera (Nikon D7100) which acquires two types of images with 3000×4496 pixels in size. Spatial resolution of the acquired images is 1.04×10^{-4} m/pixel. The camera is placed 1 m in front of the experimental chamber. We acquire bright-field [Fig. 1(a), bright] and dark-field [Fig. 1(a), dark] images of the granular packing by taking pictures without and with a second circular polarizer in front of the camera via cross-polarization mode, respectively. We carry out the experiment in a dark room to minimize ambient noise from extraneous illumination.

Each experimental run consists of the initial state followed by 1000 vertical tapings. The index of tapings τ

is defined as $\tau = N_t + 1$, where N_t is the actual tapping number. Namely, the initial condition corresponds to $\tau = 1$, and the state after one tapping is $\tau = 2$, etc. This indexing is used merely for convenience in the logarithmic data plot. The interval time between successive tapings is set to be longer than 2 s since the force-chain structure does not depend on the interval time when it is longer than 2 s. Bright-field images are acquired with every tapping, and dark-field images are taken with logarithmic intervals (i.e., $\tau = 1, 2, 3, \dots, 11, 21, 31, \dots, 101, 201, 301, \dots, 1001$). As a result, 1001 bright-field images and 29 dark-field images are obtained per experimental run. We conduct three experimental runs under identical experimental conditions to check the reproducibility of the result.

We systematically control the tapping property using the multifunction generator and the amplifier. To simply represent the ratio of the maximum tapping acceleration α_{\max} to the gravitational acceleration $g = |g| = 9.8 \text{ m/s}^2$, $\Gamma = \frac{\alpha_{\max}}{g} = \frac{A(2\pi f)^2}{g}$ is used, where f is the tapping frequency and A is the tapping amplitude which can be measured by the sinusoidal-wave fitting to the measured acceleration data, as shown in Fig. 1(c). Each particle is sufficiently released from the gravitational constraint when a chamber is shaken by $\Gamma > 2.0$ [20]. Thus, we vary the value of Γ roughly as $\Gamma = 2.5, 5.0, 10, 20$ to focus on the situation in which the particles surely experience free fall. In such situations, force-chain structure can be reorganized following each tapping. We also vary f approximately as $f = 50, 100, 200$ Hz using the multifunction generator. Figure 1(c) shows actual acceleration signals captured by the accelerometer in the case of $\Gamma = 5.0$ and $f = 50$ Hz. Due to the instrumental limitations, data with $\Gamma = 20$ and $f = 50$ Hz cannot be obtained. Accordingly, we perform experiments with $4 \times 3 - 1 = 11$ experimental conditions. In this study, we also use the normalized tapping strength S to consider the velocity balance rather than the acceleration balance between tapping amplitude and gravity. S is defined as $S = \frac{(2\pi A f)^2}{g d} = \Gamma \frac{A}{d} = \frac{\Gamma^2 g}{(2\pi f)^2 d}$ [21], where d ($= 10$ mm) is the characteristic particle diameter. By using S , various behaviors occurring in shaken granular layers can be better classified than by using Γ [22,23]. Therefore, in this study, we also use S to characterize the tapping strength. Figure 2 shows the relation between S and Γ in this study. The variation range of S is $S = 0.004\text{--}0.867$.

B. Force calibration

Force applied to a photoelastic disk can be estimated from its intensity gradient $\langle G^2 \rangle$ in dark-field images. $\langle G^2 \rangle$ denotes the mean squared intensity gradient over all pixels on the surface of a disk, and it is defined as $\langle G^2 \rangle \equiv \langle |\nabla I|^2 \rangle = \langle (\nabla I_h)^2 + (\nabla I_v)^2 \rangle$, where ∇I_h and ∇I_v are the horizontal and vertical gradients, respectively. We employ two calibration methods to compute the sum of the interparticle force per disk F_d .

The first method is the calibration with a load cell (Kyowa Electronic Instruments, LMB-A-10N) and a micrometer (Nigataseiki, MCD130-25) (Fig. 3 inset). A photoelastic disk is diametrically compressed by the micrometer. The load cell is mounted on the contact point between the disk and the micrometer. Then the photoelastic image and applied force F_d are simultaneously measured by a camera and the load

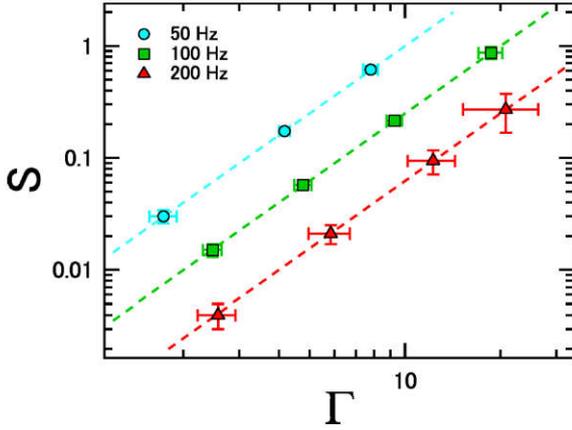


FIG. 2. Relation between S and Γ . Colors and symbols represent 50 Hz (blue circles), 100 Hz (green squares), and 200 Hz (red triangles), respectively, as shown in the legend. Error bars represent the variation over three runs under identical experimental conditions. Dashed lines are drawn in accordance with $S = \frac{\Gamma^2 g}{(2\pi f)^2 d}$.

cell, respectively, under the optical setup identical to the actual data taking [Fig. 1(b)]. Upon computing $\langle G^2 \rangle$ through image analysis, we obtain the relation between F_d and $\langle G^2 \rangle$ as shown in Fig. 3. Quadratic fits to both large and small disk data provide the calibration curves just like previous studies [24,25]. Using these calibration curves, we can estimate the force exerted on each disk by the image analysis of dark-field images.

The next calibration method concerns the detectable lower limit of F_d . The lower limit is determined by using a vertical one-dimensional (1D) chain of the same-size photoelastic disks [18]. Interparticle force per disk in the vertical 1D chain $F_d(k)$ can be estimated from the relation $F_d(k) = k \times Mg$, where k is the position of the disk from the top in the 1D chain, and

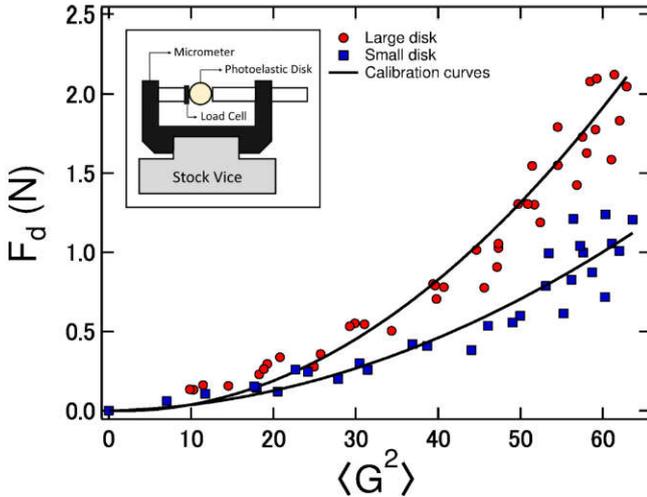


FIG. 3. Relation between F_d and $\langle G^2 \rangle$ for large (red circles) and small (blue squares) photoelastic disks. Solid lines through the calibration data are quadratic fits. (Inset) Schematic of the calibration setup. A photoelastic disk is sandwiched by the micrometer. A load cell is mounted on the contact point between the disk and the micrometer.

M is the mass per disk ($M = 1.8 \times 10^{-3}$ kg for large and $M = 0.80 \times 10^{-3}$ kg for small disks, respectively). From the calibration, $\langle G^2 \rangle$ does not vary up to $k = 2$ for large or $k = 3$ for small disks [18]. Therefore, the detectable lower limit of F_d is determined as 3.6×10^{-2} N for large and 2.4×10^{-2} N for small disks.

III. RESULTS

A. Packing fraction

We define the packing fraction ϕ as $\phi = A_d / (A_d + A_v)$, where A_d is the total area of the photoelastic disks, and A_v is the total void area between disks. The 2D packing fraction is usually calculated from the ratio between the area occupied by granular particles and the total chamber area. This definition is reasonable when the granular packing is enclosed on all sides. However, an accurate estimate of the total area of the chamber is difficult when the granular packing has a free surface. Therefore we employ the above-mentioned definition of ϕ . Figure 4(a) shows the variations of ϕ with τ for all experimental conditions. Similar to previous studies [14,15], ϕ increases with the number of tappings. The increasing rate and its asymptotic value clearly depend on the tapping strength S .

B. Deviator anisotropy

We evaluate the anisotropy of grain configurations in a compacting granular packing by using the fabric tensor and its eigenvalues. According to the previous studies [7,26], the fabric tensor $\hat{\mathbf{R}}$ in two-dimensional grain contact is defined as follows:

$$\hat{\mathbf{R}} = \frac{1}{N_p} \sum_{i \neq j}^{N_p} \frac{\mathbf{r}_{ij}}{|\mathbf{r}_{ij}|} \otimes \frac{\mathbf{r}_{ij}}{|\mathbf{r}_{ij}|}, \quad (1)$$

where N_p is the number of granular particles with two or more contact points, \mathbf{r}_{ij} is a vector heading from the center coordinate of the i th particle to the contact point with the j th particle, $|\mathbf{r}_{ij}|$ is the segment length, and \otimes expresses a vector outer product. By using the number of contact points N_c , and the x component (n_x) and y component (n_y) of the unit direction vector $\frac{\mathbf{r}_{ij}}{|\mathbf{r}_{ij}|}$, each component of $\hat{\mathbf{R}}$ is represented by the following equation:

$$\hat{\mathbf{R}} = \begin{pmatrix} \Phi_{xx} & \Phi_{xy} \\ \Phi_{yx} & \Phi_{yy} \end{pmatrix} = \frac{1}{N_c} \begin{pmatrix} \sum_{k=1}^{N_c} n_x^k n_x^k & \sum_{k=1}^{N_c} n_x^k n_y^k \\ \sum_{k=1}^{N_c} n_y^k n_x^k & \sum_{k=1}^{N_c} n_y^k n_y^k \end{pmatrix}. \quad (2)$$

Moreover, the two eigenvalues Φ_1 and Φ_2 of $\hat{\mathbf{R}}$ (in other words, Φ_1 and Φ_2 are the maximum and the minimum principal fabric components in a two-dimensional system, respectively) are calculated from the following equation:

$$\begin{pmatrix} \Phi_1 \\ \Phi_2 \end{pmatrix} = \frac{1}{2}(\Phi_{xx} + \Phi_{yy}) \pm \sqrt{\frac{1}{4}(\Phi_{xx} - \Phi_{yy})^2 + \Phi_{xy}^2}. \quad (3)$$

The anisotropy of grain contacts can generally be evaluated by the deviator of two eigenvalues $\Phi_1 - \Phi_2$ [26]. Deviator

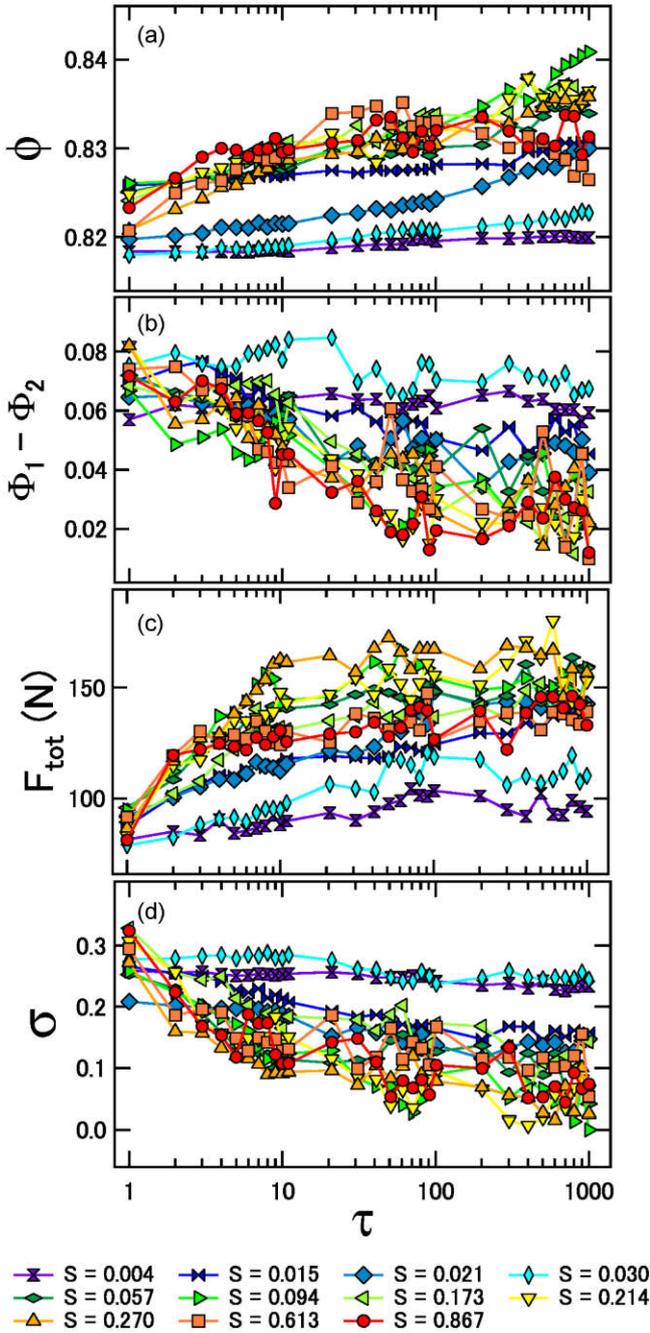


FIG. 4. Variations of (a) packing fraction ϕ , (b) deviator anisotropy $\Phi_1 - \Phi_2$, (c) total force F_{tot} , and (d) force-chain orientational order parameter σ with τ in linear-log scale. The data are averaged over three runs of the identical S and are specified by colors and symbols. Error bars are omitted to clearly show the data trend.

anisotropy $\Phi_1 - \Phi_2$ indicates the degree of anisotropy of the grain configuration. When grain contacts obey the completely isotropic configuration, $\Phi_1 - \Phi_2$ becomes 0. Figure 4(b) exhibits the relationship between $\Phi_1 - \Phi_2$ and tapping number τ in our experiment. $\Phi_1 - \Phi_2$ decreases by tappings and approaches 0. In addition, it seems that the decreasing rate depends on the tapping strength S . These results suggest that

grain configurations are evolving towards an isotropic state as tapping proceeds.

C. Interparticle force

We compute F_d in the compacted granular packing to characterize the interparticle-force behavior. In the previous work [18], we have already reported that the cumulative number distribution of F_d can be approximated by the exponential [9,10], $N_{\text{cum}}(F_d) = C_F \exp(-\frac{F_d}{F_0})$, where $N_{\text{cum}}(F_d)$ is the number of disks on which the applied force is equal to or greater than F_d . In this form, C_F and F_0 are fitting parameters. Actually, the characteristic force value F_0 varies depending on the tapping number as it approaches the asymptotic value in a few tappings [18]. However, the specific value of F_0 depends on the fitting range. Thus, in this study, we rather use the integrated value to evaluate the magnitude of internal force. Concretely, total interparticle force (F_{tot}) defined as $F_{\text{tot}} = \sum_{i=1}^{N_{\text{ch}}} F_d(i)$ is used, where N_{ch} is the number of disks composing force chains. Note that disks composing force chains are identified by the detectable limit of the photoelastic signal (Sec II B). The measured force per disk must be greater than the detectable lower limit value to form the force chain. Figure 4(c) shows the variations of F_{tot} as a function of τ for all experimental realizations. Obviously, F_{tot} increases with tapping number and approaches the asymptotic values. The asymptotic values seem to depend on the tapping strength S .

Furthermore, we also examine the force distribution per depth in the experimental chamber. In general, hydrostatic pressure determines the depth-dependent force distribution in a static fluid layer. If this simple hydrostatic nature can also be applied to the granular layer, the magnitude of contact forces should be proportional to the depth. To ascertain the hydrostatic nature determining the internal force distribution in the granular packing, we compare the sum of interparticle forces at each depth in the chamber F_{bin} and the theoretically computed hydrostatic force F_H . First, we divide the chamber into 25 horizontal slices of vertical width $\Delta z = 0.01$ m. In each slice, the sum of F_d is computed, $F_{\text{bin}}(j) = \sum_{i=1}^{N_j} F_d(i)$, where N_j is the number of disks in the j th slice. The corresponding depth of each slice $z(j)$ is defined as $z(j) = j\Delta z$. Here, $j = 0$ corresponds to the top surface of the granular layer. The corresponding hydrostatic force F_H is computed as $F_H(z) = \rho' g A z$, where $\rho' = 920$ kg m $^{-3}$ is the bulk density of the layer of photoelastic disks (in this study, we calculate $\rho' = \rho\phi't'$, where the product of the true density of the photoelastic disk is $\rho = 1.27 \times 10^3$ kg m $^{-3}$, the typical packing fraction $\phi' = 0.8$, and the thickness ratio of the disk and chamber $t' = 10/11$), and $A = 3.3 \times 10^{-3}$ m 2 is the sectional area of the chamber. The product of ρ' , g , and A is calculated as $\rho' g A = 26.9$ N/m.

Figure 5 exhibits the comparison of $F_H(z)$ and $F_{\text{bin}}(j)$ for all experimental realizations at (a) initial configuration ($\tau = 1$) and (b) final configuration ($\tau = 1001$). $F_{\text{bin}}(j)$ at $\tau = 1$ agrees well with theoretically calculated $F_H(z)$, as shown in Fig. 5(a). This result indicates that interparticle forces in a granular packing before tappings are basically governed by the hydrostatic force. However, the behaviors of $F_{\text{bin}}(j)$ at $\tau = 1001$ vary depending on S , as shown in Fig. 5(b). In the cases of $S = 0.004$ and 0.030 , $F_{\text{bin}}(j)$ still roughly obeys $F_H(z)$ even after 1000 tappings. In the case of $S \geq 0.057$, on the other

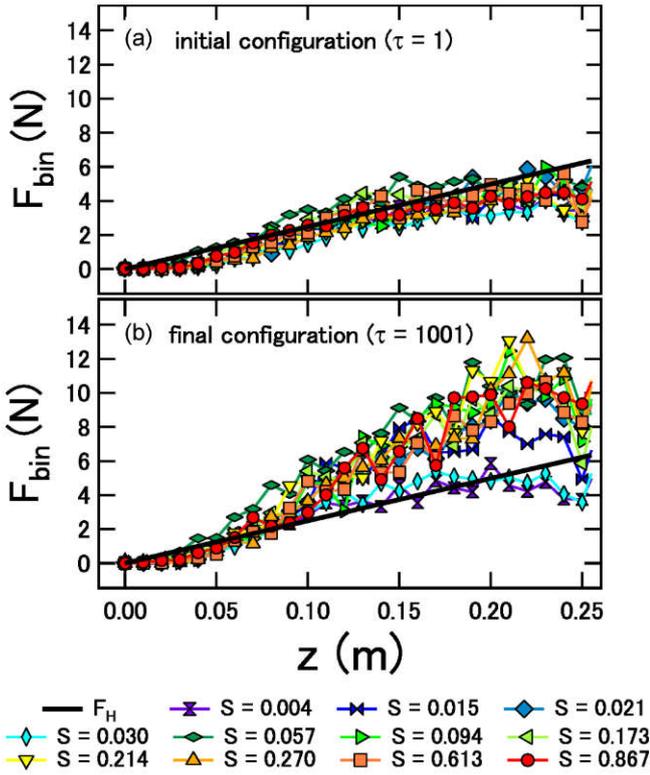


FIG. 5. Variations in F_{bin} per depth z for all experimental realizations at (a) initial configuration ($\tau = 1$) and (b) final configuration ($\tau = 1001$). The data are averaged over three runs of the identical S and are specified by colors and symbols. Error bars are omitted to clearly show the data trend. The black solid line indicates the hydrostatic force F_H per depth z .

hand, $F_{\text{bin}}(j)$ clearly increases by tapplings, particularly in the deep (large z) region.

To directly observe the increase of $F_{\text{bin}}(j)$, the two examples of actual force-chain variations by tapplings at $S = 0.867$ and $S = 0.004$ are shown in Fig. 6. In the case of $S = 0.004$, the principal force-chain structure remains unchanged during the series of tapplings as shown in Figs. 6(a)–6(d). By contrast, in the case of $S = 0.867$ [Figs. 6(e)–6(h)], one can confirm the reorganization of force-chain structure by tapplings. In addition, the thickness of bright zones with force chains seems to become thicker as tapping proceeds. The significant difference between initial and after-tapping configurations with $S = 0.867$ [Figs. 6(e)–6(h)] is the development of horizontal force-chain segments. This horizontal force-chain development is a possible reason for the increase of $F_{\text{bin}}(j)$ in the relatively deep region. The development of horizontal force chain could originate from the particle-wall friction. Such an additional constraint is necessary to understand the increase of $F_{\text{bin}}(j)$ in the deep region. In this study, it is difficult to decompose the contact force into vertical and horizontal directions because we only use $\langle G^2 \rangle$ to measure the contact force. Therefore, another method to qualify the anisotropy of the force-chain structure is necessary to discuss the tapping-induced structural variations in a force chain. To characterize the anisotropy of the force-chain structure, the order parameter of force-chain orientations could be useful.

D. Force-chain orientational order parameter

We introduce an orientational order parameter σ of the force-chain structure. Here, we define σ by using the force-chain segment length and its angle relative to the gravitational director ($\hat{g} \equiv \mathbf{g}/|\mathbf{g}|$). Specifically, σ is defined as [19]

$$\sigma = \left(\frac{2}{L} \sum_{i=1}^{N_{sg}} l_i \cos^2(\theta_i - \theta_r) \right) - 1, \quad (4)$$

where N_{sg} is the total number of force-chain segments, l_i and θ_i are length and angle of the i th segment, and $L = \sum_{i=1}^{N_{sg}} l_i$ is the total length of force-chain segments. θ_r in Eq. (4) is a reference angle. By definition, the reference axis is the same as the gravitational axis when $\theta_r = 0^\circ$, and it is perpendicular to the gravitational director in the case of $\theta_r = 90^\circ$. To measure the length of force-chain segments, the force-chain images are first thinned, and the force-chain network is divided into a collection of force-chain segments. Details of image analysis to extract the force-chain segments can be found in [18]. σ can characterize the orientational order of the force-chain structure. In the limiting cases, Eq. (4) yields $\sigma = +1$ for $\theta_i - \theta_r = 0^\circ$ (all the force chains are parallel to the reference axis) and $\sigma = -1$ for $\theta_i - \theta_r = 90^\circ$ (all the force chains are perpendicular to the reference axis). In the case of $\sigma = 0$, force-chain orientations are random (isotropic orientation) or perfectly lined up along the direction $\theta_i - \theta_r = 45^\circ$. Obviously, we can visually distinguish the difference between the isotropic random situation and perfect alignment to $\theta_i - \theta_r = 45^\circ$ for $\sigma = 0$.

In addition, we examine the behavior of σ by changing the reference axis θ_r in order to confirm that force chains are not perfectly aligned to the direction $\theta_i - \theta_r = 45^\circ$ for $\sigma = 0$. Figure 7 exhibits the tapping-induced variations of order parameter σ with various reference angles θ_r at (a) $S = 0.004$ and (b) $S = 0.867$. In Fig. 7(a), although the value of σ depends on θ_r , it does not vary on τ . On the other hand, σ in Fig. 7(b) decreases or increases depending on τ , and finally approaches to 0. Only the initial value depends on θ_r . If force-chain orientations are perfectly lined up along the direction $\theta_i - \theta_r = 45^\circ$, σ indicates 1 in the case of $\theta_r = 45^\circ$. However, the data in Fig. 7 do not show such a trend. Thus, these results suggest that force chains are not perfectly aligned to the direction $\theta_i - \theta_r = 45^\circ$ in the case of $\sigma = 0$. These results also indicate that the reference axis must be selected appropriately. In this study, the reference axis should be taken to be parallel or perpendicular to the initially dominant direction since the crucial direction (gravity director) is obvious in the current experimental system. If we use inappropriate θ_r (e.g., $\theta_r = 45^\circ$ in the current system), σ is always around 0. In this case, τ -dependent σ variation cannot be detected. When the principal direction of the system is not very obvious, θ_r dependence of σ has to be checked to clearly see the orientational ordering.

Figure 4(d) shows the variations of σ as a function of τ for all experimental realizations with $\theta_r = 0^\circ$. As tapping proceeds, σ decreases in all cases. Moreover, the decreasing rate clearly depends on the tapping strength S . The decreasing tendency of σ can qualitatively be confirmed by comparing the raw photoelastic images (Fig. 6) again. In the initial configurations [Figs. 6(a) and 6(e)], the vertical structure of force chains can

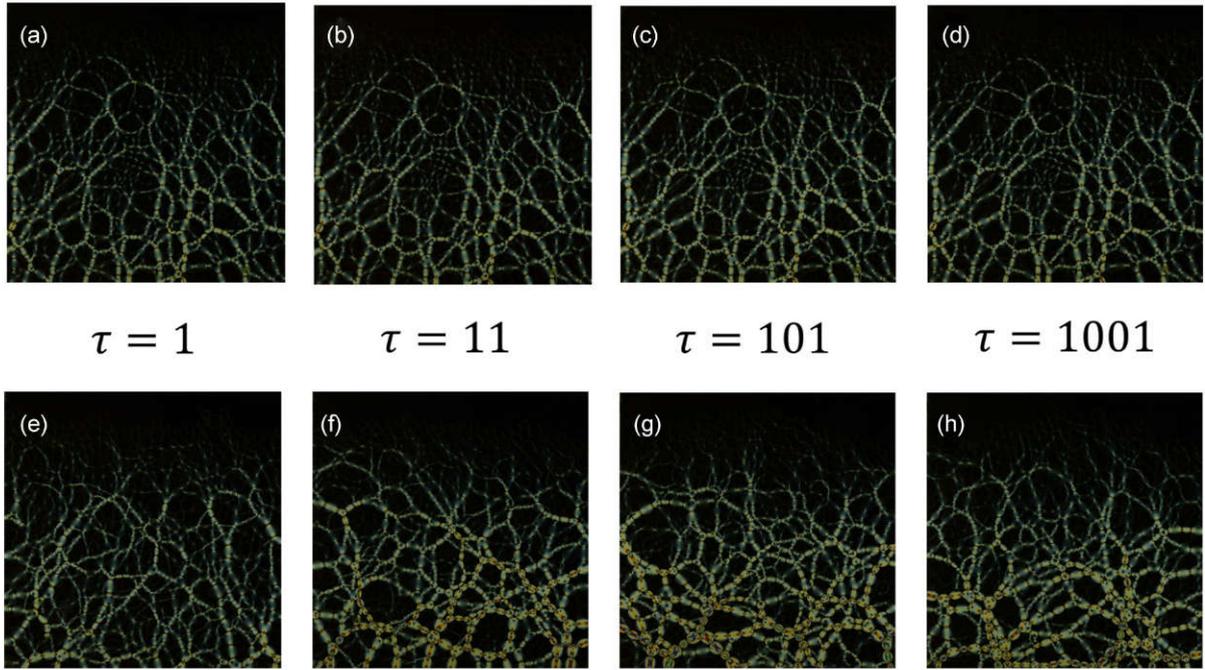


FIG. 6. Force-chain structures in various tapped configurations at (a)–(d) $S = 0.004$ and (e)–(h) $S = 0.867$.

clearly be observed. However, the way of structural evolution of force chains depends on experimental conditions. In the case of $S = 0.004$, the force chain roughly keeps the original structure even after the sufficient tapplings [Figs. 6(b)–6(d)]. In contrast, the force chains in the case of $S = 0.867$ become more random and isotropic due to the reorganization of force-chain structures caused by strong tapplings [Figs. 6(f)–6(h)]. These

tendencies of the evolution of the force-chain structure are consistent with σ behaviors.

IV. ANALYSIS AND DISCUSSION

A. Force increase mechanism

The experimental results exhibit that the increase of F_{tot} and the decrease of σ and $\Phi_1 - \Phi_2$ simultaneously occur as ϕ increases by tapplings. There are two possible ways to increase F_{tot} . One is to increase the force per particle (force-chain strengthening) and the other is to increase the number of particles composing force chains (force-chain elongation). Using the data obtained so far, we can discuss the contribution of the strengthening and elongation of the force chains.

First, F_{tot} is written by the average interparticle force F_{avg} and the total number of disks composing force chains $n (=N_{ch})$ as

$$F_{\text{tot}}(\tau) = F_{\text{avg}}(\tau)n(\tau). \quad (5)$$

Note that this relation is satisfied in every tapping stage τ . The relation between F_{tot} and F_{avg} for various S and τ is shown in Fig. 8(a). From Fig. 8(a), we can clearly confirm that F_{tot} has a linear relation with F_{avg} . In this plot, the slope corresponds to the number of disks composing force chains. From the least squares fit which crosses through the origin of the coordinate axes, $n = 349 \pm 1$ is obtained. The black line in Fig. 8(a) is the corresponding fit. This proportional relation means that the number of disks composing force chains are almost constant independent of S and τ . Since we use 600 disks in total, approximately 58% disks always construct the force-chain structure. On the other hand, the remaining 42% disks do not contribute to the force-chain formation, being ‘‘rattlers.’’ It should be noted that, however, this value could depend on the detectable lower limit of photoelasticity. According to this

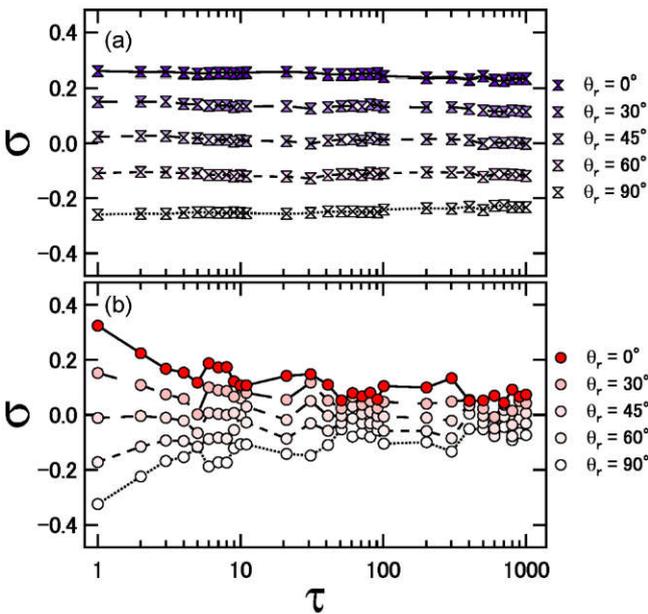


FIG. 7. Variation of order parameter $\sigma(\tau)$ at (a) $S = 0.004$ and (b) $S = 0.867$ on various reference angles θ_r in linear-log scale. The data are averaged over three runs of the identical S and are specified by colors. Error bars are omitted to clearly show the data trend.

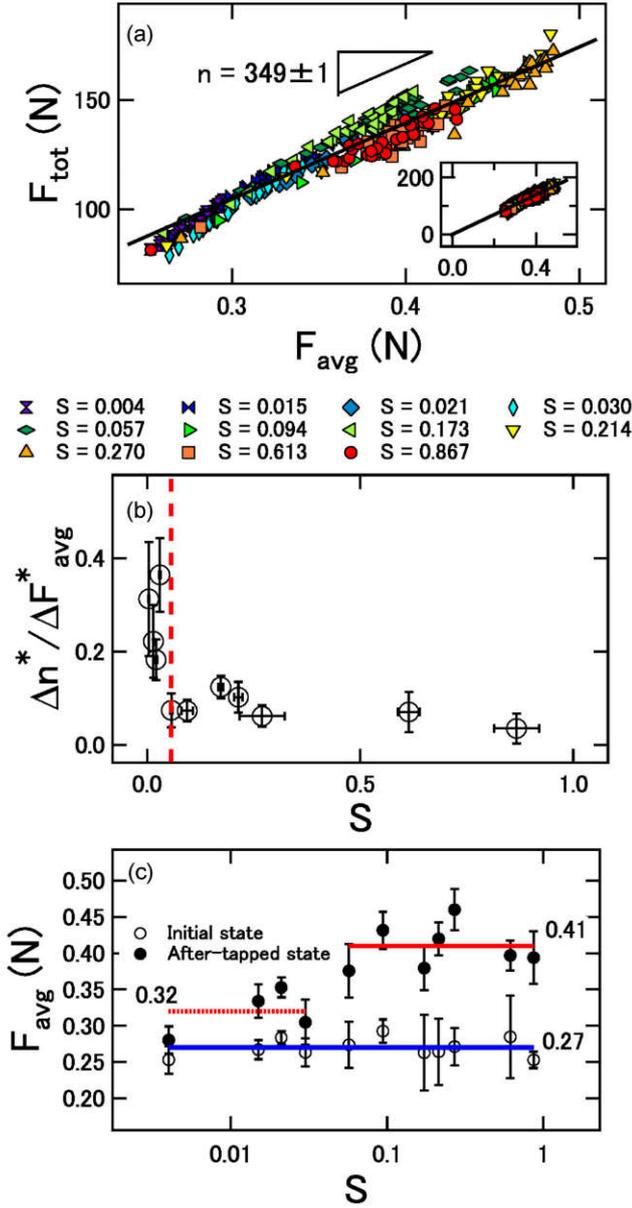


FIG. 8. (a) Relation between F_{tot} and F_{avg} . The data are averaged over three experimental runs with identical S , as specified by colors and symbols. Error bars are omitted to clearly show the data trend. The black solid line indicates the linear fitting to all data. (Inset) data and the fit line are displayed including the origin of the coordinate axes. (b) Variations of $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ as a function of S . The data points are obtained by averaging all τ data. Error bars represent the standard deviation. The vertical red dashed line indicates $S = 0.057$ above which the convective motion can be observed. (c) Initial (hollow symbol) and after-tapped (black filled symbol) values of F_{avg} as a function of S . Error bars represent the standard deviation. Blue solid line is the average of the initial values under all experimental conditions. Red dotted and solid lines are the averages of the after-tapped values at $S \leq 0.030$ and $S \geq 0.057$, respectively.

result, the principal effect increasing F_{tot} must be the increase of F_{avg} rather than the elongation of force chains because n , the number of particles belonging to the force chains, seems to be constant.

To confirm this, we proceed with quantitative characterization of the increment of F_{tot} in the following. In order to evaluate the contribution of F_{avg} and n to the increment of F_{tot} , we have to normalize them since they have different dimensions. These quantities are normalized to their initial values as, $\Delta F_{\text{avg}}^*(\tau) = \frac{F_{\text{avg}}(\tau) - F_{\text{avg}}(1)}{F_{\text{avg}}(1)}$, and $\Delta n^*(\tau) = \frac{n(\tau) - n(1)}{n(1)}$. The normalized increment of F_{tot} can also be represented by the same form as $\Delta F_{\text{tot}}^*(\tau) = \frac{F_{\text{tot}}(\tau) - F_{\text{tot}}(1)}{F_{\text{tot}}(1)}$. Equation (5) can be rewritten by using their initial values and the differences from the initial value [$\Delta F_{\text{tot}}(\tau) = F_{\text{tot}}(\tau) - F_{\text{tot}}(1)$, $\Delta F_{\text{avg}}(\tau) = F_{\text{avg}}(\tau) - F_{\text{avg}}(1)$, and $\Delta n(\tau) = n(\tau) - n(1)$] as

$$\Delta F_{\text{tot}}(\tau) = F_{\text{avg}}(1)\Delta n(\tau) + n(1)\Delta F_{\text{avg}}(\tau) + \Delta F_{\text{avg}}(\tau)\Delta n(\tau). \quad (6)$$

Furthermore, by dividing both sides of Eq. (6) by $F_{\text{tot}}(1)$, we obtain the relation among ΔF_{tot}^* , ΔF_{avg}^* , and Δn^* :

$$\Delta F_{\text{tot}}^* = \Delta n^* + \Delta F_{\text{avg}}^* + \Delta F_{\text{avg}}^* \Delta n^*. \quad (7)$$

All the values of ΔF_{avg}^* and Δn^* obtained in this study are less than unity. Therefore we neglect the higher-order terms $\Delta F_{\text{avg}}^* \Delta n^*$. Then, the simple relation among ΔF_{tot}^* , ΔF_{avg}^* , and Δn^* can be obtained from Eq. (7) as

$$\Delta F_{\text{tot}}^* \approx \left(1 + \frac{\Delta n^*}{\Delta F_{\text{avg}}^*}\right) \Delta F_{\text{avg}}^*, \quad (8)$$

where $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ indicates the relative contribution of the increment of n compared with the contribution of the F_{avg} increment. Thus, we can evaluate the contribution of F_{avg} and n to the increment of F_{tot} by examining the specific value of $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$.

Here, we investigate S dependence of $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ since the tapping strength S would influence the force-chain structure as mentioned in Sec. III D. The computed S dependence of $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ is shown in Fig. 8(b). In the very small S regime ($S = 0.004$ – 0.030), we can confirm $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*} \simeq 0.2$ – 0.4 . In this parameter range, the variations of ϕ , F_{tot} , and σ by tappings are quite small (Fig. 4). In other words, it is not easy to compact the granular packing by such weak tapping. By contrast, the contribution of force-chain elongation in this regime is relatively greater than that in the larger S regime ($S \geq 0.057$). In the relatively large S regime, $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ becomes about 0.1. The difference of $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ depending on S can be interpreted by Figs. 8(a) and 8(c). Figure 8(a) indicates that the number of disks constituting the force chains does not substantially depend on S . In fact, the value of Δn^* shows approximately 0.08 almost independent of S . On the other hand, interparticle force increases depending on S . To focus on the amount of increase in F_{avg} from the initial value, we indicate the difference between the initial and after-tapped values of F_{avg} on Fig. 8(c). As after-tapped values of F_{avg} , we use the average values of F_{avg} during all the tapping states other than the initial value. The initial average value of F_{avg} for all experimental conditions is 0.27 N [Fig. 8(c)]. In the after-tapped states, the average value of F_{avg} in the small S regime ($S = 0.004$ – 0.030) is about 0.32 N, while F_{avg} in the large S regime ($S \geq 0.057$) is approximately 0.41 N. From these results, ΔF_{avg}^* is 0.19 in the small S regime and 0.52 in

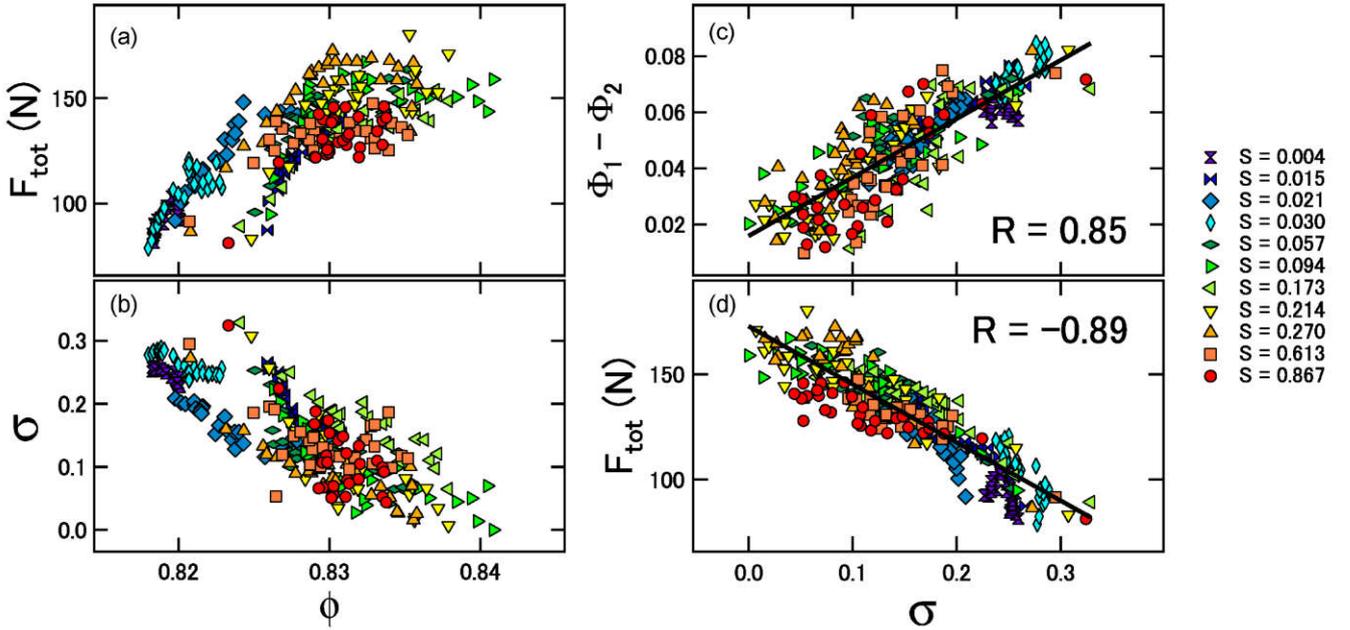


FIG. 9. Relations among ϕ , $\Phi_1 - \Phi_2$, F_{tot} , and σ : (a) F_{tot} vs ϕ , (b) σ vs ϕ , (c) $\Phi_1 - \Phi_2$ vs σ , and (d) F_{tot} vs σ . The data are averaged over three experimental runs of the same S , as specified by colors and symbols. Error bars are omitted to clearly show the data trend. The black solid lines in (c) and (d) indicate the linear fittings. $R = 0.85$ in (c) and $R = -0.89$ in (d) denote the correlation coefficients for the relations $\Phi_1 - \Phi_2$ vs σ and F_{tot} vs σ , respectively.

the large S regime. For all experimental conditions, the average value of Δn^* is approximately 0.08, so that $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ indicates 0.42 in small S and 0.15 in large S regimes. These values almost agree with the values of the respective regions in Fig. 8(b). Altogether, in the tapping processes, the force-chain elongation effect could be almost negligible, although interparticle force increases depending on tapping strength S .

Actually, the increase of F_{tot} can also be observed for the force-chain evolution in an isotropic compression and shear [6,24]. Moreover, the length of the force chain does not change under an isotropic compression and shear [27,28]. Thus, the observed result in the tapped granular packing is basically similar to other loading cases, at least in the large S ($S \geq 0.057$) regime.

B. Relations among four parameters

We next investigate the relations among ϕ , $\Phi_1 - \Phi_2$, F_{tot} , and σ . The relations among these quantities are shown in Fig. 9. Figure 9(a) clearly indicates that F_{tot} increases as ϕ increases and finally saturates at the asymptotic value around $F_{\text{tot}} \simeq 150$ N. This saturation tendency has not been observed in an isotropic compression and shear loading [4,5]. We consider that this saturation tendency results from the steady particle motions. When a granular packing is vertically shaken by tapping, each particle could move and form the convective motion [16]. Then, particle motions cause the decrease of interparticle forces (loosening) even near ϕ_{RCP} [11]. In this state, the particle motions and compaction are balanced to form the steady state in terms of F_{tot} variation.

In order to check the actual particle motions in the current experiment, we track the particle traces. Figure 10 shows the traces of actual particle motions during 100 tapplings from

$\tau = 901$ to $\tau = 1001$ at (a) $S = 0.030$ and (b) $S = 0.613$. Figure 10(b) exhibits that the particle motions clearly form a pair of convective rolls, while particles are almost at rest in the case of small S [Fig. 10(a)]. We observe that the particle motions drastically change beyond $S = 0.057$. This threshold for the onset of convective motion corresponds to that for the drastic change of $\frac{\Delta n^*}{\Delta F_{\text{avg}}^*}$ [Fig. 8(b), red dashed line]. This S threshold also distinguishes the qualitative behavior of ϕ , $\Phi_1 - \Phi_2$, F_{tot} , and σ : very slow compaction or rapid compaction followed by saturation (Fig. 4). In the convective (large S) regime, this behavior could be natural since the particle configurations are actively reorganized by convection. In the small S ($S \leq 0.03$) regime, F_{tot} basically shows the gradual increase by tapping since the convective motions cannot be observed.

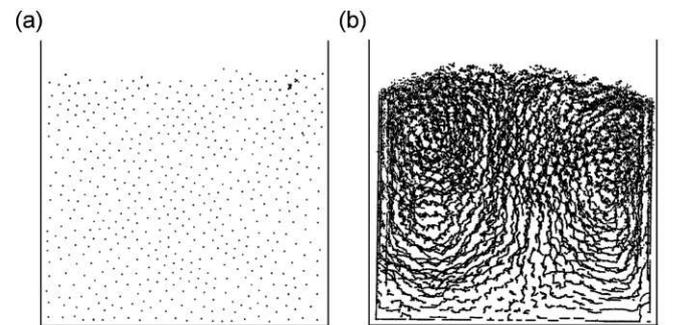


FIG. 10. Particle-motion traces at (a) $S = 0.030$ and (b) $S = 0.613$ during 100 tapplings from $\tau = 901$ to $\tau = 1001$: (a) particles are almost at rest and (b) particle collective motions form a pair of convective rolls.

In this study, we do not report on the further quantitative characterization of the convective motion. In addition, the physical meaning of the threshold value $S = 0.057$ has not been revealed in this study. The detailed analysis of convective motions observed in this experimental system and a comparison of the result with the three-dimensional case (e.g., [29]) will be presented elsewhere.

With respect to the relation between σ and ϕ , Fig. 9(b) exhibits that σ approaches 0 as ϕ increases. This tendency can robustly be observed in the convection state. The convective roll structure does not affect the force-chain structure. Even in the small S regime, the force-chain structure gradually becomes isotropic without significant reconfiguration. Only the reorganization of the contact network can also produce isotropic force-chain structure. This result agrees with our previous study in which the force-chain structure monotonically approaches an isotropic state by tappings [19].

Next, we compare $\Phi_1 - \Phi_2$ and σ . $\Phi_1 - \Phi_2$ indicates the isotropy of grain configuration in granular packing, and σ characterizes the orientational order of the force-chain structure. The relation between grain configurations and force-chain structures does not necessarily correspond with each other since about 40% of disks are rattlers and do not contribute to the force-chain formation.

Figure 9(c) exhibits the relation between $\Phi_1 - \Phi_2$ and σ . The least squares fitting is used to obtain the correlation coefficient R . The fitting result is shown as the black solid line in Fig. 9(c). The computed correlation coefficient $R = 0.85$ shows that $\Phi_1 - \Phi_2$ has a positive correlation with σ . This correlation could mean that the isotropy of the orientational order of the force-chain structure comes from the isotropy of grain configuration. That is, the disordering of grains contact and force-chain structure occur simultaneously.

Finally, we investigate the relation between F_{tot} and σ [Fig. 9(d)]. The black solid line in Fig. 9(d) shows the fitting result. The computed correlation coefficient $R = -0.89$ indicates that σ has a clear negative correlation with F_{tot} . This clear negative correlation indicates that the linear relationship universally holds in the wide range of S regardless of particle motions with or without convection.

A recent study has reported that the force-chain structure becomes homogeneous when the three-dimensional (3D) granular packing is compressed by an uniaxial loading [12]. This experiment has shown that the force distribution under the

uniaxial external loading becomes homogeneous even when particles are not able to form convective motion. Although the relation between the force-chain orientational order in a 2D system and force homogeneity in a 3D system is still unclear, they might have a certain relation with each other. Further studies with various loading conditions under various spatial dimensions are important future issues to be investigated.

V. CONCLUSIONS

In this study, we have experimentally investigated the evolution of a 2D force-chain structure in a compacted granular packing by adding vertical tappings. We have measured the fabric tensor, interparticle forces, and force-chain orientational order parameter. The tapping-induced granular compaction is also measured by the packing fraction. The experimental results demonstrate that the interparticle force increases, whereas the deviator anisotropy derived from the fabric tensor and the orientational order parameter of force chains decreases as the packing fraction increases due to the compaction. In contrast, the total length of force-chain segments remains almost constant during compaction. A positive correlation has been observed between the deviator anisotropy and orientational order of the force-chain structure. This relation claims that origins of isotropy of force-chain orientational order and grain configurations could be identical. Both quantities can similarly characterize the isotropy in a granular packing. Moreover, a clear negative correlation is universally observed in any tapping strength between interparticle force and orientational order of the force-chain structure. This result indicates that large interparticle forces and isotropic force-chain structure are simultaneously realized in the compacted granular packing near the random close packing state.

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